



# Mechanical Vibrations



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Eng. Laith Batarseh

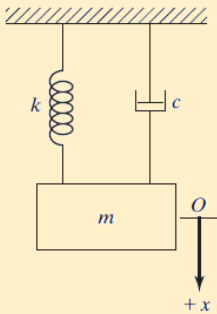
## Single DoF free vibration system



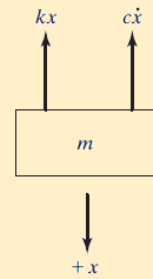
### Single DoF free damped vibration system

#### System free body diagram

C is the damping constant or coefficient



System



Free-body diagram

# Single DoF free vibration system



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## Single DoF free damped vibration system

Mathematical model (governing equation)

$$m \ddot{x} + c \dot{x} + kx = 0$$

**Solution:**

$$ms^2 + cs + k = 0 \quad \Rightarrow \quad s_{1,2} = \frac{-c \pm \sqrt{c^2 - 4mk}}{2m}$$

Characteristic equation

$$s_{1,2} = -\frac{c}{2m} \pm \sqrt{\left(\frac{c}{2m}\right)^2 - \frac{k}{m}}$$

# Single DoF free vibration system



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## Single DoF free damped vibration system

**Critical damping ( $c_c$ )**

The critical damping  $c_c$  is defined as the value of the damping constant  $c$  for which the radical in s-equation becomes zero:

$$\left(\frac{c_c}{2m}\right)^2 - \frac{k}{m} = 0 \Rightarrow c_c = 2m\sqrt{\frac{k}{m}} = 2m\omega_n$$

**damping ratio ( $\zeta$ )**

$$\zeta = \frac{c}{c_c} = \frac{c}{2m\omega_n}$$

So:

$$s_{1,2} = \left(-\zeta \pm \sqrt{\zeta^2 - 1}\right)\omega_n$$

# Single DoF free vibration system



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## Single DoF free damped vibration system

$$s_{1,2} = \left( -\xi \pm \sqrt{\xi^2 - 1} \right) \omega_n$$

### Case 1: under-damped system ( $\zeta < 1$ )

$$s_{1,2} = \left( -\xi \pm i\sqrt{1 - \xi^2} \right) \omega_n$$

$$x(t) = e^{-\xi\omega_n t} \left\{ C_1 \cos\left(\sqrt{1 - \xi^2} \omega_n t\right) + C_2 \sin\left(\sqrt{1 - \xi^2} \omega_n t\right) \right\}$$

$$x(t) = X_o e^{-\xi\omega_n t} \left\{ \sin\left(\sqrt{1 - \xi^2} \omega_n t + \phi_o\right) \right\}$$

$$x(t) = X e^{-\xi\omega_n t} \left\{ \cos\left(\sqrt{1 - \xi^2} \omega_n t - \phi\right) \right\}$$

# Single DoF free vibration system



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### Case 1: under-damped system ( $\zeta < 1$ )

$$x(t=0) = x_o = C_1$$

Assume I.C.s:

$$\dot{x}(t=0) = \dot{x}_o \Rightarrow C_2 = \frac{\dot{x}_o + \xi\omega_n x_o}{\sqrt{1 - \xi^2} \omega_n}$$

$$x(t) = e^{-\xi\omega_n t} \left\{ x_o \cos\left(\sqrt{1 - \xi^2} \omega_n t\right) + \frac{\dot{x}_o + \xi\omega_n x_o}{\sqrt{1 - \xi^2} \omega_n} \sin\left(\sqrt{1 - \xi^2} \omega_n t\right) \right\}$$

# Single DoF free vibration system

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## Case 1: under-damped system ( $\zeta < 1$ )

The constants  $X$ ,  $X_o$ ,  $\phi$  and  $\phi_o$  can be expressed as:

$$X = X_o = \sqrt{C_1^2 + C_2^2} = \frac{\sqrt{x_o^2 \omega_n^2 + \dot{x}_o^2 + 2x_o \dot{x}_o \xi \omega_n}}{\sqrt{1 - \xi^2} \omega_n}$$

$$\phi_o = \tan^{-1} \left[ \frac{C_1}{C_2} \right] = \tan^{-1} \left[ \frac{x_o \omega_n \sqrt{1 - \xi^2}}{\dot{x}_o + \xi \omega_n x_o} \right]$$

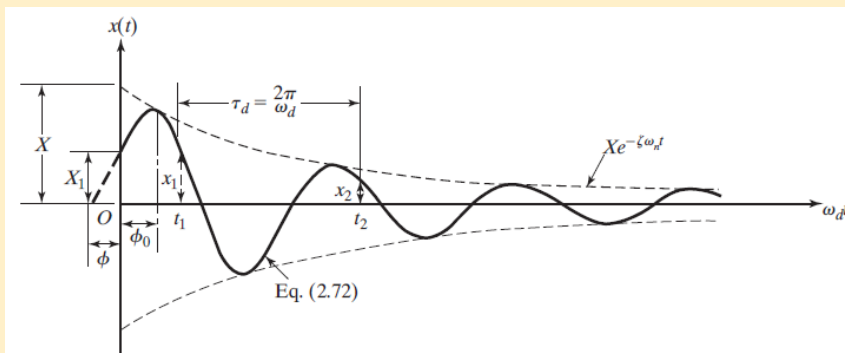
$$\phi = \tan^{-1} \left[ \frac{C_2}{C_1} \right] = \tan^{-1} \left[ \frac{\dot{x}_o + \xi \omega_n x_o}{x_o \omega_n \sqrt{1 - \xi^2}} \right]$$

# Single DoF free vibration system

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## Case 1: under-damped system ( $\zeta < 1$ )

Frequency of damped vibration:  $\omega_d = \sqrt{1 - \xi^2} \omega_n$



Under-damped solution

# Single DoF free vibration system



## Single DoF free damped vibration system

### Case 2: critically damped system ( $\zeta=1$ )

$$s_{1,2} = -\omega_n$$

$$x(t) = e^{-\omega_n t} \{C_1 + C_2 t\}$$

$$x(t=0) = C_1 = x_o$$

$$\dot{x}(t=0) = \dot{x}_o \Rightarrow C_2 = \dot{x}_o + \omega_n x_o$$

$$x(t) = e^{-\omega_n t} \left\{ x_o + \left( \dot{x}_o + \omega_n x_o \right) t \right\}$$

# Single DoF free vibration system



## Single DoF free damped vibration system

### Case 3: overdamped system ( $\zeta > 1$ )

$$s_{1,2} = \left( -\zeta \pm \sqrt{\zeta^2 - 1} \right) \omega_n < 0$$

$$x(t) = C_1 e^{-(\zeta + \sqrt{\zeta^2 - 1})\omega_n t} + C_2 e^{-(\zeta - \sqrt{\zeta^2 - 1})\omega_n t}$$

$$x(t=0) = x_o \Rightarrow C_1 = \frac{x_o \omega_n (\zeta + \sqrt{\zeta^2 - 1}) + \dot{x}_o}{2\omega_n \sqrt{\zeta^2 - 1}}$$

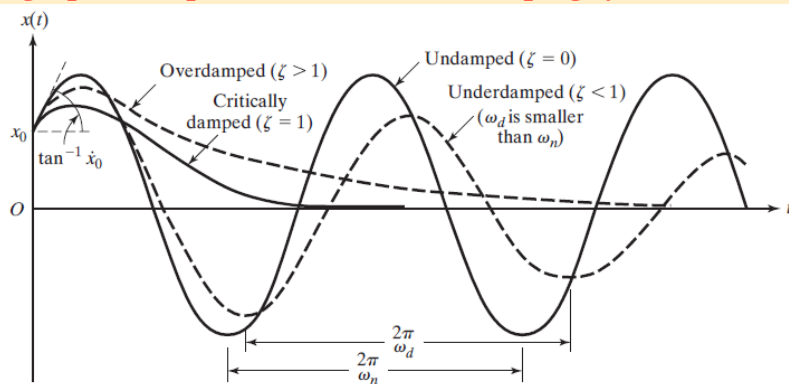
$$\dot{x}(t=0) = \dot{x}_o \Rightarrow C_2 = \frac{-x_o \omega_n (\zeta - \sqrt{\zeta^2 - 1}) - \dot{x}_o}{2\omega_n \sqrt{\zeta^2 - 1}}$$

# Single DoF free vibration system

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## Single DoF free damped vibration system

The graphical representation for the damping systems

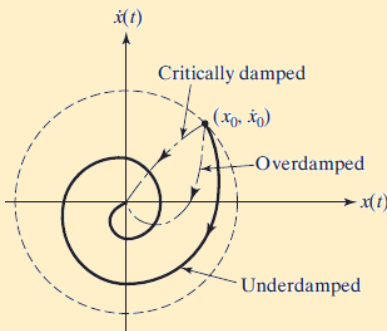


# Single DoF free vibration system

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## Logarithmic decrement

The logarithmic decrement represents the rate at which the amplitude of a free-damped vibration decreases. It is defined as the natural logarithm of the ratio of any two successive amplitudes.



Phase plane of a damped system.

# Single DoF free vibration system

VIBRATION

**Logarithmic decrement**

$$\frac{x_1}{x_2} = \frac{X_o e^{-\xi\omega_n t_1} \cos(\omega_d t_1 - \phi_o)}{X_o e^{-\xi\omega_n t_2} \cos(\omega_d t_2 - \phi_o)}$$

**So**

$$\frac{x_1}{x_2} = \frac{e^{-\xi\omega_n t_1}}{e^{-\xi\omega_n (t_1 + \tau_d)}} = e^{\xi\omega_n \tau_d}$$

**But**

$$t_2 = t_1 + \tau_d \Rightarrow \tau_d = \frac{2\pi}{\omega_d}$$

$$\cos(\omega_d t_2 - \phi_o) = \cos(2\pi + \omega_d t_1 - \phi_o) = \cos(\omega_d t_1 - \phi_o)$$

**Assume:  $\delta$  the logarithmic decrement**

$$\delta = \ln \frac{x_1}{x_2} = \xi\omega_n \tau_d = \xi\omega_n \frac{2\pi}{\sqrt{1-\xi^2}\omega_n} = \frac{2\pi\xi}{\sqrt{1-\xi^2}} = \frac{2\pi}{\omega_d} \cdot \frac{c}{2m}$$

**Logarithmic decrement: is dimensionless**

# Single DoF free vibration system

VIBRATION

**Logarithmic decrement**

$$\xi = \frac{\delta}{\sqrt{(2\pi)^2 + \delta^2}}$$

**For small damping ;  $\zeta \ll 1$**

$\delta \approx 2\pi\xi$

# Single DoF free vibration system



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## Example 2.6

An under-damped shock absorber is to be designed for a motorcycle of mass 200 kg (Fig.(a)). When the shock absorber is subjected to an initial vertical velocity due to a road bump, the resulting displacement-time curve is to be as indicated in Fig.(b).

### Requirements:

1. Find the necessary stiffness and damping constants of the shock absorber if the damped period of vibration is to be 2s and the amplitude  $x_1$  is to be reduced to one-fourth in one half cycle (i.e.  $x_{1.5} = x_1/4$  ).

# Single DoF free vibration system

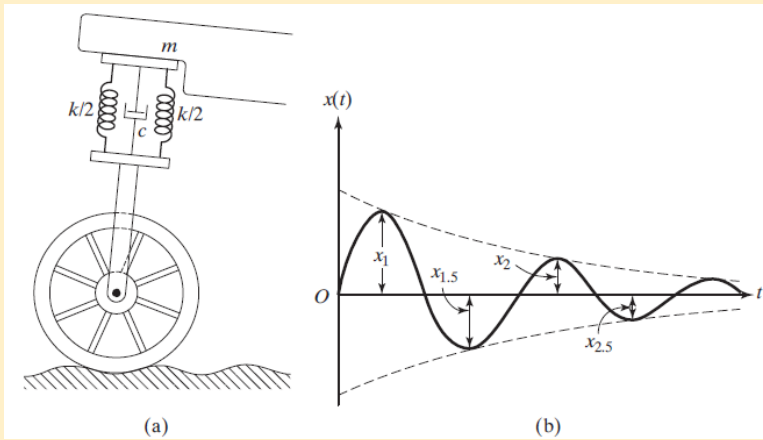


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## Example 2.6

Note that this system is under-damped system





## Single DoF free vibration system



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### Example 2.6

**Solution:**

**Finding k and c**

Since  $x_{1.5} = x_1/4$ ,  $x_2 = x_{1.5}/4 = x_1/16$  and so, the logarithmic decrement become:

$$\delta = \ln \frac{x_1}{x_2} = \ln(16) = 2.7726 = \frac{2\pi\xi}{\sqrt{1-\xi^2}}$$

$$\Rightarrow \xi = 0.4037$$

**Hence:**

$$\tau_d = 2 = \frac{2\pi}{\omega_d} = \frac{2\pi}{\omega_n \sqrt{1-\xi^2}} \Rightarrow \omega_n = \frac{2\pi}{\omega_n \sqrt{1-0.4037^2}} = 3.4338 \text{ rad/s}$$



## Single DoF free vibration system



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### Example 2.6

**Solution:**

**Finding k and c [cont]**

The critical damping can be found as:

$$c_c = 2m\omega_n = 2(200)(3.4338) = 1373.54 \text{ N-s/m}$$

And so the damping constant can be found as:

$$c = \xi c_c = (0.4037)(1373.54) = 554.4981 \text{ N-s/m}$$

And stiffness can be found as:

$$k = m\omega_n^2 = (200)(3.4338)^2 = 2358.2652 \text{ N/m}$$



## Single DoF free vibration system



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End of chapter